

APPLICATION
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TITLE: **ADAPTIVE POWER AMPLIFIER SYSTEM**

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SPECIFICATION

ADAPTIVE POWER AMPLIFIER SYSTEM

Related Application

This application claims the filing benefit and priority of U.S. Provisional Application entitled "Adaptive Power Amplifier with Variable Outputs," Serial No. 60/273,746,; filed March 6, 2001, and incorporates that application by reference herein in its entirety.

Field of the Invention

The present invention generally relates to a power amplifier system used in telecommunication systems and more specifically to an adaptive system for efficiently combining and transmitting signals created by one or more power amplifiers.

Background of the Invention

Wireless communication signals received by antennas are often very weak. Therefore, power amplifiers are widely used in wireless

frequency if an SCPA were to fail. Therefore, a level of redundancy is desirable for MCPAs implemented within a power amplifier scheme of a transmission system. Such a system of redundancy would also be useful in SCPA systems. Such redundancy would ensure that all of the carrier signals are not lost due to a single amplifier failure.

It is also often desirable to increase the number of carriers that may be amplified by an SCPA system. Such a system must allow additional SCPAs to be easily added to the power amplifier system.

Within a wireless transmission system, it is often desirable to upgrade or modify the system by adding additional amplification. Since the output power is increased by either replacing existing power amplifiers or adding additional amplifiers, such a system must allow for easy replacement of existing MCPAs or SCPAs or allow for the addition of more MCPAs or SCPAs.

When providing or modifying the amplification features of a wireless system to address such objectives, one possible solution is to construct a combining network consisting of multiple power amplifiers, which also allows additional amplifiers to be added. It also should provide for the amplifiers to be easily removed and replaced if necessary. However, several obstacles must be overcome in order for such a network to be cost effective and efficient.

First, the impedance of the output line of a combiner will vary depending upon the amplifiers in the system. Therefore, the system must address the issue of varying line characteristics at the output of a signal combiner, such as the impedance of the output line, based upon the

number of MCPAs or SCPAs inserted within the system. This is an important consideration in order to ensure an efficient transfer of the amplified signals from the signal combiner to the output lines.

Additionally, a system with multiple ports for accepting power amplifiers will experience various levels of input signal loss if any of the ports are empty. Therefore, a solution to the above objectives must address input signal losses based upon the number of ports containing power amplifiers within the system.

Still further considerations involve the types of components utilized in the signal combining network. Conventional systems with multiple power amplifiers often use a large number of switches in order to control the flow of input signals to the various amplifiers. Such switches have various drawbacks. First, switches are inherently lossy electrical devices. Therefore, signal strength decreases each time a signal passes through a switch. Secondly, since switches are mechanical devices, they have a certain degree of unreliability because they are prone to failure. Therefore, a solution to various of the above-discussed issues should also address such unreliability, switch failures, minimize signal loss from switching components, and improve the robustness of the overall system.

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constructed according to one embodiment of the present invention. The RF input signal 102 may be provided to the amplifier module 100 from an antenna, from a transmission line, or from any other suitable electronic circuitry. The RF signal 102 is received by a variable amplifier 104 and then forwarded to input signal splitter circuitry 106 that divides the input signal into separate signals directed to a number of available ports capable of accepting power amplifiers. The divided input signal is then routed to the power amplifiers and sensor circuit 108 that contains the plurality of ports into which power amplifiers may be inserted. The sensor circuit 108 generates a control signal that is routed to a microprocessor controller 114 when power amplifiers are inserted or removed. The amplified output signal of each power amplifier is then forwarded to a signal combiner and output circuitry 110 that combines the signals from the power amplifiers creating a summed output signal 112. The controller 114 is also coupled to the output circuitry 110 and routes the summed output signal 112 through the appropriate output circuitry 110 according to the sensed occupancy level of power amplifiers within the amplifier module 100 as indicated by the control signal received from the sensor circuit 108. In that way, output characteristics of the line are taken into consideration and the output signal 112 is routed for maximum power transmission and efficiency. That is, a router will effectively route the output signal based upon parameters associated with the number of amplifiers. In one embodiment, the router includes a controller with various inputs and outputs and associated circuitry.

The amplification applied to the RF input signal 102 by the variable amplifier 104 is also controlled by the controller 114. The amplification level is dependent upon the number of power amplifiers detected by the controller 114 and will be discussed in more detail below.

A more detailed description of the operation of one embodiment of the invention is set forth below in relation to Figures 2 and 3. Figure 2 depicts an amplifier module with various aspects of the invention, that contains four ports 200-1, 200-2, 200-3, 200-4, each of which is capable of accepting a power amplifier 202. An amplifier module 100 according to the present invention is not limited to having four power amplifiers. A system capable of handling fewer power amplifiers or many more may be realized in accordance with the present invention. The description of the embodiment herein is directed to a system with four power amplifier ports for illustrative purposes only to explain the various aspects of the present invention.

In the embodiment shown in Figure 2, the input RF signal 102 is fed into the variable amplifier 104. A connection between the variable amplifier 104 and the microprocessor controller 114 is depicted in Figure 2 as VA. Figure 3 depicts the controller 114 with connections for VA and sensor circuit nodes 1, 2, 3, and 4 and switching circuit nodes A, B, C, and D which will be discussed in more detail below.

Returning to Figure 2, the output of the variable amplifier 104 is divided by an input signal splitter 106 and the signals are routed to four ports 200-1, 200-2, 200-3, 200-4 present within the amplifier module 100. In one embodiment, the input signal splitter 106 is comprised of three

Wilkinson splitter networks 204. Other acceptable methods for splitting the input signal may also be used. The operation and method for building Wilkinson splitter networks is well known in the art and is described in "An N-Way Hybrid Power Divider" by E. J. Wilkinson, *IRE Transactions on Microwave Theory and Techniques*, Vol. MTT-8, No. 1, January 1960. The outputs of the final stage of Wilkinson splitter networks 204 are coupled with the input side of the power amplifier ports 200-1, 200-2, 200-3, 200-4.

If a port 200 does not contain a power amplifier 202, then the portion of the original RF input signal 102 routed to that port is essentially lost. This phenomenon is known as "split loss." In the preferred embodiment, which contains four ports, if a power amplifier is inserted into only one port, then three-fourths of the original RF input signal 102 will be lost. If two ports contain power amplifiers, then one-half of the original RF input signal will be lost, and so on. However, if all four ports contain a power amplifier, then little or no portion of the original input signal will be lost. The variable power amplifier 104 compensates for any "split losses" by amplifying the RF input signal 102 to ensure the full signal strength of the original RF input signal is received by each power amplifier 200.

In accordance with one aspect of the present invention, the number of amplifiers being utilized is monitored. Using a sensor circuit, the controller 114 determines the number of power amplifiers 202 inserted within the ports 200. As the number of power amplifiers 202 inserted within ports 200 increases, the controller 114 decreases the amplification level of the variable amplifier 104 using the control line VA. If the number

source 218. The controller 114 is coupled to the insert detection circuits 212 at the sensor circuit nodes identified as 1, 2, 3 and 4 in Figure 2. When a power amplifier is inserted into a port 200, such as the top-most power amplifier port 200-1, a voltage is generated at node 1 at the detection circuit 212. This voltage is in the form of a control signal that is detected by the controller 114. By detecting this voltage, the controller 114 determines that a power amplifier 202 has been inserted into the port and the port 200-1 is now occupied. Similarly, if a power amplifier 202 is inserted into the second port 200-2, a voltage control signal is generated at node 2 of the insert detection circuit 212, and the controller 114 determines that a second amplifier has been inserted in that respective port. The same occurs at nodes 3 and 4 if power amplifiers 202 are inserted into ports 200-3 or 200-4. If any power amplifier 202 is removed from any one of ports 200-1, 200-2, 200-3 or 200-4, then the voltage at the corresponding node 1, 2, 3 or 4 in the insert detection circuits 212 drops. The controller 114 detects this drop in voltage at the appropriate node and then determines that fewer ports 200 are occupied by power amplifiers.

The use of multiple insert detection circuits as described above is only one method for providing a sensor that indicates when power amplifiers are inserted or removed from the ports 200 of the amplifier module 100. A single sensor may be used to generate a control signal that corresponds to the number of ports 200 containing a power amplifier 202. For instance, insert detection circuitry 212 as described above may be fed into digital circuit components. This digital circuitry may then

The output lines 220 in each contain a first transmission line segment 222-1, 222-2, 222-3 or 222-4 of a specific length and characteristic impedance. In the disclosed embodiment, for example, the first transmission line segments 222 have a length $\lambda/4$ and impedances of 50, 35.35, 28.88 and 25 ohms, respectively. From the combiner, the segments 222 terminate at nodes A, B, C, or D. Second transmission line segments 224 of length $\lambda/4$ and an impedance of 50 ohms, are also coupled to the nodes A, B, C, and D. A grounding switch 226 is coupled between a ground contact and the nodes connecting the two transmission

line segments. In the disclosed embodiment, the grounding switches 226 are of the single-pull single-throw type (SPST); however, a variety of different switch types and/or additional transmission line segments may be used to accomplish the function of creating conditions of high and low impedance, as discussed below.

The first transmission line segment 222 in each output line 220 is used to modify the electrical line characteristics of the respective output lines 220. In one embodiment, the impedance of transmission line segment 222 is varied between each of the different output lines 220. In accordance with one aspect of the invention, the impedance value of each transmission line segment 222-1, 222-2, 222-3 and 222-4 is selected so that the effective impedance presented at nodes A, B, C, and D shown in Figure 2 is transformed to generally match the impedance of the second output transmission line segments 224, which is 50 ohms. To accomplish this, the impedance values for transmission line segments 222-1, 222-2, 222-3 and 222-4 are selected as one of multiple geometric means between the 50 ohm impedance value of the second output transmission line segment 224 and the various parallel impedance combinations of the number of ports 200 which contain power amplifiers. Depending on the number of amplifiers used, the parallel impedance of the amplifier ports will vary.

For instance, in the disclosed embodiment, if only one of the ports 200 is occupied by a power amplifier, then the effective impedance presented to the input of combiner 208 is 50 ohms. Therefore, to transform this impedance value to match the 50 ohm impedance of the

second output transmission line segment 224 at a node (A, B, C, D) the first output transmission line segment 222 must have an impedance value which is the geometric mean of the 50 ohm impedance at the combiner input and the 50 ohm impedance of segment 224, i.e., 50 ohms. This corresponds specifically to segment 222-1 and node A.

If two ports 200 contain power amplifiers 202, then the impedance presented to the input of the combiner 208 is the parallel combination of 50 ohms and 50 ohms, i.e., 25 ohms. The impedance value of the output transmission line segment 222 is then selected as the geometric mean between 25 and 50 ohms, which is approximately 35.35 ohms. This corresponds to segment 222-2 and node B.

Similarly, if three ports contain power amplifiers, then the combined parallel impedance at the input to combiner 208 is 16.67 ohms, resulting in a value of 28.88 ohms selected as the impedance for output transmission line segment 222-3 and node C. If four power amplifiers are inserted into ports 200, then the impedance value for output transmission line segment 222-4 associated with node D is 25 ohms.

If a power amplifier system is designed to accept more than four power amplifiers, additional output lines can be coupled to the combiner 208 and the necessary impedance values for the first transmission line section 222 calculated according to the method and principles described above.

As discussed above, the controller 114 monitors the voltages at nodes 1, 2, 3 and 4 shown in Figure 2 in order to determine whether a power amplifier has been inserted into one or more of the ports 200.

Based upon the number of power amplifiers detected, the controller 114 sets the grounding switches 226 located at switching circuit nodes A, B, C and D to the appropriate positions as will be described in more detail below.

In operation, adaptive power amplifier module 100 operates as follows. For example, assuming a single power amplifier is inserted into port 200-1, the impedance at the input to the combiner 208 is 50 ohms. Using the sensor circuitry 212, the controller 114 detects a voltage control signal at sensor node 1, indicating a single power amplifier is present. No control signals are sensed at the other nodes. With a 50 ohm impedance at the combiner, it is desirable to have the output of the combiner routed to line segment 222-1. This will yield an effective impedance at node A of 50 ohms.

To effect the routing to segment 222-1, the controller 114 closes the grounding switches 226 located at nodes B, C and D. Closing the switches grounds the nodes and causes the associated $\lambda/4$ lines 222-2, 222-3 and 222-4 and 224 coupled to these switches to effectively become deactivated. At a $\lambda/4$ away from the grounded nodes, they are transformed into open circuits (i.e., high impedance) both at the output of combiner 208 and at the output 228 of the power amplifier module. On the other hand, the controller activates output transmission line segment 222-1 by causing the switch 226 at node A to be opened, or remain open. Therefore, the summed output signal from the combiner 208 will propagate through the 50 ohm, $\lambda/4$ output transmission line segment 222-1 to be output at the power amplifier module output 228.

In another example, assume power amplifiers are inserted into ports 200-1 and 200-2. Their combined impedance at the combiner 208 is 25 ohms. The controller 114 would detect voltage control signals at sensor nodes 1 and 2 as shown in Figure 2 indicating two power amplifiers are present as 200-1, 200-2. The desirable transmission line segment is then 222-2 which is reflective of a geometric mean of 25 ohms and 50 ohms. The controller 114 then causes the grounding switches 226 at nodes A, C, and D to be closed while the switch 226 at node B would be opened. The closed switches cause the $\lambda/4$ lines 222-1, 222-3, 222-4, and 224 associated with the nodes A, C and D to be deactivated and transformed into open circuits (i.e., high impedance) both at the output of the combiner 208 and at the power amplifier module output 228. The summed output signal from combiner 208 will then propagate from the output of the combiner 208 through the activated output transmission line segment 222-2 which has an impedance of 35.35 ohms. The 25-ohm impedance that was presented to this path at the combiner 208 is transformed via the 35.35-ohm, $\lambda/4$ line 222-2 to an impedance of 50 ohms at node B. The impedance remains 50 ohms as it transitions through the 50-ohm, $\lambda/4$ transmission line segment 224 to the output of the power amplifier module 228.

The same basic operation occurs when three or four power amplifiers are inserted into ports 200. The appropriate signal path when three power amplifiers are inserted is through node C and line segment 220-3, and the appropriate signal path when four power amplifiers are inserted is through node D and line segment 220-4. Selecting the correct

path ensures that the impedance from the combiner 208 to the output 228 is effectively transformed to approximately 50 ohms.

A power amplifier system as described above generally requires the use of only one switch per output line. Therefore, the total number of switches required by the system is greatly reduced. Furthermore, since the output lines are activated or deactivated by connecting the output lines to ground via the switches, the summed output signal from the combiner 208 is never required to propagate through a switch. Therefore, the switching operation of the present invention reduces the undesirable signal loss and reliability concerns that exist when multiple switches are used.

Figures 4A and 4B illustrate additional embodiments of the invention, wherein additional transmission line segments are utilized with switches 226 to achieve a desired selection of an output transmission line segment. Figures 4A and 4B illustrate alternative embodiments of the invention for one of the nodes, Node A. It will be readily understood that similar alternative embodiments may be utilized for the other nodes, as well, or any number of nodes utilized in accomplishing the present invention.

Referring to Figure 4A, utilizing switch 226, it physically may not be able to achieve the desired closed circuit/ low impedance, or open circuit/high impedance characteristics at the node. Therefore, an alternative embodiment is illustrated in Figure 4A, and an additional transmission line segment 230 may be utilized. In making the transmission line segment 230 a 50 ohm $\lambda/4$ segment, the effect on the node A from the closing of switch 226 will be an opposite effect from the

effect of the embodiment as illustrated in Figure 2. That will then also lead to an opposite effect at a distance $\lambda/4$ from node A. Therefore, in order to activate the $\lambda/4$ line 222-1, rather than leaving the switch 222 open, the switch is closed. The closed switch then translates into a high impedance at node A, but an effective low impedance at both the output of the combiner 208 and at the output 228 of the power amplifier module. Similarly, if node A is the chosen path for the output, to deactivate the other lines, the switches are left open, translating into a low impedance at each of the respective nodes, and then a high impedance at the output of combiner 208 for each of the lines. Therefore, in the example discussed above wherein one power amplifier is present, the switch 226 associated with node A is closed, wherein the other switches remain open. Similar selective closing and opening of switches 226 may be utilized to select other nodes for the output of the combiner 208.

Figure 4B illustrates still another alternative embodiment which would effectively operate similarly to the embodiment illustrated in Figure 2. However, an additional transmission line segment 232 is utilized in combination with switch 226 to physically achieve a desired circuit. Transmission line segment 232 is, however, $\lambda/2$ in length, and therefore, the condition at the switch 226 is realized directly at the node, such as node A. That is, as discussed with respect to the embodiment illustrated in Figure 2, the closing of switch 226 will deactivate a particular output line and node, wherein leaving the switch open will select a particular output line and node for routing the output of the combiner 208.

In the present invention, any port 200 that does not contain a power amplifier is terminated as an open-circuit impedance by operation of a switch 226 or switch/line segment combination. This impedance is transformed, via the 50-ohm, $\lambda/2$ segment of transmission line 206, to the combiner 208 as an open circuit. This open circuit condition will have no impact on the overall impedance presented to the combiner 208 until a power amplifier is coupled. Therefore, amplifier modules with large numbers of unoccupied ports may be installed to accommodate for future growth. A new amplifier may be added at anytime, and the adaptive power amplifier module 100 will automatically adjust its operation, as described above, to ensure efficient operation.

Further, the selection of the appropriate output line 220-1, 220-2, 220-3 or 220-4 by the controller 114 is not affected by which particular ports 200 contain power amplifiers. The controller 114 needs to know that ports are occupied by power amplifiers; however, knowledge about which ports are occupied is irrelevant. Therefore, this system does not require power amplifiers to be installed in any particular one of ports 200 in any particular order. A power amplifier can be installed in any port 200 of the power amplifier module 100 and create identical performance.

A further feature of the preferred embodiment is that the switches 226 at nodes A, B, C and D may be "hot switched." That is, power amplifiers can be inserted into any one of the ports 200 without having to power down the RF input signal 102. The typical lifetime of these switches when hot switching is used is limited to several operations. If the RF input 102 to the module 100 is powered down for a few milliseconds during

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insertion of a power amplifier (to power levels of less than 25 dBm), the lifetime of these switches may be several million operations. Typically, these switches will see no more than 10-20 operations during their lifetime.

The adaptive power amplifier system described herein may be implemented to operate in a wide variety of frequency bands. Examples of the frequencies in which the preferred embodiment may be operated include cellular, the European 1800 MHz Digital Communication System (DCS), Personal Communication System (PCS), Universal Mobil Telecommunications System (UMTS), and Multichannel Multipoint Distribution System (MMDS) frequencies.

The descriptions of the preferred embodiments described above are set forth for illustrative purposes and are not intended to limit the present invention in any manner. Equivalent approaches are intended to be included within the scope of the present invention. While the present invention has been described with reference to the particular embodiments illustrated, those skilled in the art will recognize that many changes and variations may be made thereto without departing from the spirit and scope of the present invention. These embodiments and obvious variations thereof are contemplated as falling within the scope and spirit of the claimed invention.